

Numerical analysis of discs based on carbon-nanofiber/Al₂O₃ZrO₂ nanocomposite materials

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ABSTRACT: In this study, the behavior of three different discs consisting of AS4 carbon fiber, T-300 carbon, and Al₂O₃ZrO₂ (nanocomposite) materials at constant temperature was investigated by the numerical analysis method. Nanocomposites are formed by the dispersion of nanometer-sized particles in a matrix. With the advantages that nanocomposites bring to the material, they increase heat resistance in general. Carbon fibers, on the other hand, are preferred in the aerospace and aircraft industries due to their high strength properties. In this study, it was assumed that the modulus of elasticity does not change with temperature. The temperatures applied to the discs are 45 °C, 60 °C, 75 °C, 90 °C, and 105 °C, respectively. It has been observed that the radial and tangential stress values obtained at high temperatures are higher than at low temperatures. The Al₂O₃ZrO₂ nanocomposite materials have found that the stresses occurring in the Al₂O₃ZrO₂ (nanocomposite) disc are higher than the stresses occurring in the AS4 carbon fiber disc. The stresses obtained on the AS4 carbon fiber disc are T-300 carbon discs.

KEYWORDS: Al₂O₃ZrO₂ (nanocomposite); AS4 carbon fiber; T-300 carbon; elastic stress analysis

1. Introduction

Discs are very important for machine parts. Recently, knowledge of the tensile behavior of discs made of different materials has been considered indispensable for high-temperature machines. Discs have many practical engineering applications, such as in reciprocating and centrifugal compressors, gas and steam turbine rotors, internal combustion engines and turbojet engines, and fly wheels. A brake disc can be an example of a solid rotating disc where only body force is involved. Solid discs can also be found in components such as cover plates for rotating components and idlers used in belt assemblies^[1,2]. The thermal analysis of discs is an important issue because of their many practical applications in mechanical engineering.

As an example, in a study conducted, the thermoelastic stresses of rotating discs of variable thickness were investigated. A correlation has been established between thickness and stress^[3]. Thermal analysis is a primordial stage in the study of brake systems because the temperature determines the thermomechanical behavior of the structure^[4]. Composite materials are used in various fields because they have a long service life, high strength, and low weight. In general, they have recently been preferred in the aviation industry. Carbon fibers, on the other hand, are resistant to corrosion in aviation. In addition, their sensitivity is low despite fatigue cracking^[5–7]. The studies conducted in the literature on the production and characterization of alumina-zirconia and other nanocomposite laminates are quite

limited. Some recent studies published in the literature reveal some of the results obtained for composite ceramic laminates^[8,9]. When different studies are examined, it is understood that the zircon-reinforced nanocomposite shows high strength compared to other materials^[10].

In the other study, steel dampers on a wall panel consisting of square-section frames subjected to a hot rolling process were examined by numerical analysis. The data obtained at the end of the study were processed in the literature. In addition, it has emerged as a result that elastic stiffness is formed at an optimal level^[11]. The stresses occurring at different angles of different shock absorbers, accompanied by different temperatures, were studied. At the end of the study, it was found that there is a relationship between temperature and sample strength^[12]. In different studies, the elastic angular velocities occurring in the annular disc have been determined. In addition, the results obtained at the end of elastic analyses on rotating circular discs with different properties have been shared with the literature with graphs^[13,14].

In another study, the thermomechanical properties of a functionally rated mounted uniform disc with a rigid body/without a body were investigated. The results obtained were compared with each other^[15]. In the other study, the estimation of the bending and out-of-plane loading effects on the formability response of steel plates was examined. The results obtained are considered to reveal good results for the literature^[16]. The materials used in this study are of vital importance. For example, carbon nanofiber shows the continuous, high strength found in filament counting shots. The material is processed as a high-tensile, PAN-based fiber^[17]. Nanocarbon fibers are used in areas requiring high strength; they have different sizes in different forms^[18]. Carbon-Nanofiber/Al₂O₃ZrO₂ Nanocomposite Materials: Al₂O₃ZrO₂ Nanocomposite Material materials are used as catalysts or catalyst supports, oxygen sensors, solid electrolytes, membranes, and high-temperature thermal insulation^[19,20]. Alumina (Al₂O₃) is an exceptional ceramic structure known for its unique optical, mechanical, and electrical properties. The strength of Al₂O₃ and Al₂O₃-based ceramics can be enhanced by the application of strategic techniques that may include the inclusion of secondary phase particles (such as zirconia and ZrO₂)^[21]. T-300 carbons: carbon fiber can be preferred, especially in the bumper parts of ultra-luxury vehicles. Carbon fiber is the most suitable material for weight reduction studies^[22,23].

This study is a numerical study, and the mechanical properties of carbon nanofiber/ $Al_2O_3ZrO_2$ nanocomposite materials have been processed in a computer program developed only through mathematical modeling. The results obtained were found to be compatible with the literature. In general, to give information about the production method of nanocomposites and the distribution of reinforced materials to the matrix in an experiment that can be performed at later stages, the need of human society to build low-weight, high-strength, and durable structures has increased the demand for composite materials. In a different study, the effects of carbon nanotubes on the thermal behavior of epoxy resin composites were investigated.

At the end of the study, it was shown that the thermal stability of epoxy composites is directly related to the increase in the percentage of CNTs, as the CNT content increases to 75.0% by weight and the thermal decomposition temperature of epoxy composites increases by 75 °C. In addition, it has been observed that energy absorption increases by 6.0% in CNTs, with an increase of up to 14.4% by weight^[24]. In a different study, carbon nanotube-reinforced composite honeycomb sandwich panels were made using silicone molding. During the study, different amounts of nanotubes were added to the epoxy resin to determine the role of carbon nanotubes on the pressure and bending behavior of sandwich panels. The results reveal the conclusion that the compressive strength of honeycomb panels has a direct relationship with the increase in the percentage of carbon nanotubes and the thickness of the wall. For example, when

the compressive strength of sandwich panels increases from 42 MPa to 54 MPa, carbon nanotubes increase from 0.025% to 0.075% by weight^[25].

In addition to all these and some other studies conducted in the literature^[26–28], there are still visible problems in this area, and more research is needed, so in this study, thermal elastic stress analysis was performed under constant temperature.

2. Material and method

In this study, thermal elastic stresses occurring at temperatures of 45 °C, 60 °C, 75 °C, 90 °C, 105 °C were determined (**Figure 1**).



Figure 1. Discs exposed to elastic stress.

Analytical solution

For the composite thin disc, reference can be made to the fact that the plane stress state prevails, i.e., the stresses perpendicular to the plane do not act. σ_r and σ_{θ} are coefficients of radial and tangential thermal expansion. It shows the constants of the $a_{\theta\theta} a_{rr}$ heavy-elasticity matrix. Here, the expressions of elasticity constants in terms of engineering constants are as follows^[29]. **Figure 2** shows the modeled disc subjected to thermal stress.



Figure 2. A disc consisting of different materials subjected to thermal stress analysis.

$$a_{\theta\theta} = \frac{1}{E_{\theta}} \tag{1}$$

$$a_{\rm rr} = \frac{1}{E_{\rm r}} \tag{2}$$

$$a_{r\theta} = \frac{-\upsilon_{r\theta}}{E_r} \tag{3}$$

Equilibrium equation for plane stress case,

$$\frac{r(d\sigma_r)}{dr} + (\sigma_r) - (\sigma_\theta) + R = 0$$
(4)

It is given in the form. If the mass force R is neglected,

$$k^2 = \frac{a_{\rm rr}}{a_{\theta\theta}} \tag{5}$$

For the general equilibrium equation^[29] in the form. The equilibrium equation in which the stress function can be defined as F is as follows:

$$r^{2}F'' + rF' - k^{2}F = \frac{(\alpha_{r} - \alpha_{\theta})T}{a_{\theta\theta}}r - \frac{a_{\theta\theta}T'}{a_{\theta\theta}}r^{2}$$
(6)

r is the radius of the disc at any point, σ_r is the radial stress, and σ_{θ} is the tangential stress. Change of variables $r = e^t$ can be made. For constant temperature, it can be written as $T = T_0$. Radial and tangential stresses are written as follows:

$$\sigma_{\rm r} = \frac{\rm F}{\rm r} \tag{7}$$

$$\sigma_r = C_1 r^{k-1} + C_2 r^{-k-1} + A \tag{8}$$

$$\sigma_{\theta} = \frac{\mathrm{dF}}{\mathrm{dr}} \tag{9}$$

$$\sigma_{\theta} = C_1 k r^{k-1} - C_2 k r^{-k-1} + A$$
(10)

the integration constants C_1 , C_2 and the final term A are determined as follows:

$$A = \frac{(\alpha_r - \alpha_\theta) T_0}{a_{\theta\theta} (1 - k^2)}$$
(11)

$$C_1 = A \frac{a^{k+1} - b^{k+1}}{b^{2k} - a^{2k}}$$
(12)

$$C_2 = A \frac{a^{2k}b^{k+1} - b^{2k}a^{k+1}}{b^{2k} - a^{2k}}$$
(13)

Figure 2 shows the disc exposed to thermal stress.

During the analysis, it was assumed that the mechanical properties of composite materials do not change at high temperatures.

3. Findings and discussion

In this study, the distributions of the stress components in the elastic region of three different composite discs consisting of AS4 carbon fiber, T-300 carbon, and $Al_2O_3ZrO_2$ (nanocomposite) were calculated. The disc is fixed, and its dimensions are taken as a = 20 mm, c = 100 mm. Solutions were obtained using temperature values of 45 °C, 60 °C, 75 °C, 90 °C, and 105 °C. The properties of the materials of composite discs are given in **Table 1**^[30-32].

Table 1. The stress components of a composite disc with different materials in the elastic region^[30–32].

Materials	\mathbf{E}_{Θ}	Er	k	α _r	α_{Θ}	$\upsilon_{_{\Theta}r}$
AS4 carbon fiber	235,000	15,000	3.94	-0.5×10^{-6}	15×10^{-6}	0.20
T-300 carbon	230,000	15,000	3.91	-0.7×10^{-6}	12×10^{-6}	0.20
Al ₂ O ₃ ZrO ₂ (nanocomposite)	310,000	310,000	1.00	-12.66×10^{-6}	-12.66×10^{-6}	0.22

Temperature	Surface	AS4 carbon fiber		T-300 carbon		Al ₂ O ₃ ZrO ₂ (nanocomposite)	
Δ <i>T</i> (°C)		σt (MPa)	σr (MPa)	σt (MPa)	σr (MPa)	σt (MPa)	σr (MPa)
45 °C	Inner (r = 20)	33.563	0.00	32.849	0.00	44.275	0.00
	Outer (r = 100)	-19.543	0.00	-19.127	0.00	-25.780	0.00
60 °C	Inner (r = 20)	67.126	0.00	65.698	0.00	88.549	0.00
	Outer (r = 100)	-39.086	0.00	-38.254	0.00	-51.560	0.00
75 °C	Inner (r = 20)	100.689	0.00	98.547	0.00	132.824	0.00
	Outer (r = 100)	-58.628	0.00	-57.381	0.00	-77.339	0.00
90 °С	Inner (r = 20)	134.252	0.00	131.396	0.00	177.098	0.00
	Outer (r = 100)	-78.171	0.00	-76.508	0.00	-103.119	0.00
210 °C	Inner (r = 20)	313.255	0.00	306.590	0.00	413.230	0.00
	Outer (r = 100)	-182.399	0.00	-178.518	0.00	-240.611	0.00

The stresses of the discs are given in **Table 2**.

Table 2. The radial stress occurs in the elastic region of the disc.

In **Figure 3**, the radial stress occurring in the AS4 carbon fiber material disc is given. It can be seen in this figure that for the AS4 carbon fiber disc in 3, the radial stress (r = 46.4 mm) on the inner surface of the disc at 45 °C was 5.44 MPa.



Figure 3. Radial stress occurs in the elastic region of AS4 carbon fiber disc.

It was observed that the radial stress at the innermost part of the disc (r = 46.4 mm) at a temperature of 90 °C was 66.39 MPa. It has been determined that the radial stresses are in the form of compression stress, and the disc has the highest value in the r = 40.8 mm region. Tangential stresses occurring in the elastic region of the AS4 carbon fiber disc are displayed in **Figure 4**.



Figure 4. Tangential stress occurs in the elastic region of AS4 carbon fiber disc.

While the tangential stress on the inner surface of the disc at 45 °C was 33.56 MPa, it was observed that the tangential stress in the innermost part of the disc at 90 °C was 134.25 MPa. It has been determined that the tangential stresses are in the form of compression stress up to the region of r = 57.6 mm. From this region of the disc to the outermost part of the r = 100 mm disc, the stresses regularly increase as tensile stress.

In Figure 5, the radial stresses occurring in the elastic region of the T-300 carbon disc are displayed.



Figure 5. Radial stress occurs in the elastic region of the T-300 carbon disc.

It can be seen in this figure that the radial stress on the inner surface of the disc was at 45 °C (r = 46.4 mm), while it was 9.28 MPa. It was observed that the radial stress at the innermost part of the disc (r = 46.4 mm) at a temperature of 90 °C was 64.98 MPa. It has been determined that the radial stresses are in the form of compression stress, and the disc has the highest value in the r = 40.8 mm region.

In Figure 6, the tangential stresses occurring in the elastic region of the T-300 carbon disc are displayed.



Figure 6. Tangential stress occurs in the elastic region of the T-300 carbon disc.

While the tangential stress on the inner surface of the disc at 45 °C was -32.84 MPa, it was observed that the tangential stress in the innermost part of the disc at 90 °C was 131.39 MPa. It has been determined that the tangential stresses are in the form of compression stress up to the region of r = 57.6 mm. From this region of the disc to the outermost part of the r = 100 mm disc, the stresses regularly increase as tensile stress.

In **Figure 7**, the radial stresses occurring in the elastic region of the $Al_2O_3ZrO_2$ (nanocomposite) disc are displayed.



Figure 7. Radial stress occurs in the elastic region of Al₂O₃ZrO₂ (nanocomposite) disc.

It can be seen in this figure that the radial stress on the inner surface of the disc was at 45 °C (r = 46.4 mm), while it was 12.51 MPa. It was observed that the radial stress at the innermost part of the disc (r = 46.4 mm) at a temperature of 90 °C was 87.59 MPa. It has been determined that the radial stresses are in the form of compression stress, and the disc has the highest value in the r = 40.8 mm region.

In **Figure 8**, the tangential stresses occurring in the elastic region of the Al₂O₃ZrO₂ (nanocomposite) disc are displayed.



Figure 8. Tangential stress occurs in the elastic region of the Al₂O₃ZrO₂ (nanocomposite) disc.

In the case of **Figure 8**, the tangential stresses occurring in the elastic region of the $Al_2O_3ZrO_2$ (nanocomposite) disc are shown. While the tangential stress on the inner surface of the disc at 45 °C was 44.27 MPa, it was observed that the tangential stress in the innermost part of the disc at 90 °C was 177.09 MPa. It has been determined that the tangential stresses are in the form of compression stress up to the region of r = 56.8 mm, and the stresses increase in the case of tensile stress from this region of the disc to the outside. It has been determined that the results of the elastic analysis performed on discs made of different materials are similar to the findings obtained in this study. This is comparable with the literature^[18–21]. In **Figure 9** below, the tangential stresses obtained at a temperature of 210 °C are shown in a single graph.



Figure 9. Showing the tangential stresses occurring at a temperature of 210 °C on a single graph.

In their study, Apatay and Eraslan^[33] examined the radial and tangential stress and displacement changes that occur in the disc by giving the effect of both mechanical load and thermal load to a rotating disc. According to the results he obtained, the radial stresses are always zero at the innermost and outermost parts of the disc. Tangential stresses, on the other hand, are always greater than radial stresses^[33]. As shown in Figures 3–9, the radial stresses in the innermost and outermost regions of the discs are always zero in all graphs. The intensity of tangential stress is greater than that of radial stress. The findings obtained coincide with the studies in the literature^[34,35]. When the graphs between **Figures** 3-9 are examined, it is seen that there are increases in the intensity of radial and tangential stresses with temperature deceleration. This study shows similarities with other studies obtained in the literature^[36,37]. The stresses obtained on the disc with $Al_2O_3ZrO_2$ (nanocomposite) material are greater than the stresses calculated on the disc with AS4 carbon fiber material. The stresses obtained on the disc with AS4 carbon fiber material are higher than the stresses obtained on the disc with T-300 carbon material. In other words, the disc with Al₂O₃ZrO₂ (nanocomposite) material has the largest stresses. The T-300 carbon disc has the lowest stress. The main reason for this situation is that the mechanical properties of the materials are different. In addition, the modulus of elasticity of $Al_2O_3ZrO_2$ (nanocomposite) material is quite high compared to other materials. The modulus of elasticity is directly related to the stresses that occur. Similarly, in a different study^[38], it was found that the stresses obtained in materials with different moduli of elasticity are different from each other.

In **Figure 9**, it is seen that the tangential stress occurring in the $Al_2O_3ZrO_2$ (nanocomposite) disc is higher than in discs with other materials.

4. Conclusion

In this study, elastic thermal stresses were formed by an analytical method. The constant distribution of temperature is taken into account.

Radial and tangential stress components occurring in various temperature distributions from the inner surface to the outer surface of discs consisting of $Al_2O_3ZrO_2$ (nanocomposite), AS4 carbon fiber, and T-300 carbon materials increase with temperature.

It is also clear from this study that if the temperature is constant in each region of the disc, radial stresses occur in the form of compressive stress.

Tangential stresses occur as compression stresses.

The stresses obtained in the disc with $Al_2O_3ZrO_2$ (nanocomposite) material are higher than the stresses obtained in the disc with AS4 carbon fiber material.

The stresses calculated on the AS4 carbon fiber material disc is higher than the stresses calculated on the T-300 carbon disc.

It is high in stresses obtained at very high temperatures. For example, the tangential stress obtained on the inner surface of the $Al_2O_3ZrO_2$ (nanocomposite) disc at 210 °C is 413.22 MPa.

Conflict of interest

The author declares no conflict of interest.

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